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Emily Tsz Yan WONG/PLAND

寄件者: tmylwdpo_pd/PLAND
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副本: Emily Tsz Yan WONG/PLAND
主旨: 轉寄: A/YL-TYST/1326補充資料
附件: DD121 LOT551唐人新村 FS Drawing 16092025.pdf; 搬遷戶原址位置.pdf; A-YL-TYST-1326 Drainage Proposal 7-1-2026.pdf

From: tpbpd/PLAND <tpbpd@pland.gov.hk>
Sent: Wednesday, January 7, 2026 11:24 AM
To: tmylwdpo_pd/PLAND <tmylwdpo@pland.gov.hk>
Cc: Kiff Kit Fu YIU/PLAND <kkfyiu@pland.gov.hk>
Subject: Fw: A/YL-TYST/1326補充資料

From: 陳灝然 [REDACTED]
Sent: Wednesday, January 7, 2026 11:14 AM
To: tpbpd/PLAND <tpbpd@pland.gov.hk>
Cc: Edwin Wai Shing YEUNG/PLAND <ewsyeung@pland.gov.hk>
Subject: A/YL-TYST/1326補充資料

敬啟者

此電郵取代今日09:14發出的電郵。

有關上述檔案現提供補充資料。

發展局

搬遷戶原址為：

DD125 LOT 1490RP、1492RP(部份)、1503RP(部份)、1505S.A (部份)、1505RP(部份)、1506 (部份)、1512、1513 (部份)、1514 (部份)、1520 (部份)、1521 (部份)、1522。

附件為搬遷戶原址位置圖。

消防署

附件為消防建議。

渠務署

附件為渠務建議。

環保署

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第一，場地存放的建築材料包括：磚石、玻璃、水泥等，不會產生塵埃，不會對環境有影響。



第二，場地洗手間是臨時式廁所，會有便槽，便槽底部空間供儲存糞便，儲存容量為600升。作業者會定期聘請專業技術人員進行吸糞工作，所有污水皆獨立儲存在流動洗手間內。

北



連接線
MATCH LINE
第十張
SHEET 10

搬遷戸原址位置

第十七張
SHEET 17
連接線
MATCH

DD125

DD124

連接線
MATCH LINE
第十六張
SHEET 16

連接線
MATCH LINE
第十二張
SHEET 12 117

第四張

SHEET 4
連接線
MATCH

1. GENERAL

- ## 2. HOSE REEL SYSTEM

- ### 3. AUTOMATIC SPRINKLER SYSTEM

- #### 4. FIRE ALARM SYSTEM

- ## 5. EMERGENCY LIGHTING

- ## 6. EXIT SIGN

- ## 7. PORTABLE APPLIANCES

- 7.1 PORTABLE HAND OPERATED APPLIANCES SHALL BE PROVIDED AS INDICATED ON PLAN.



 BREAK GLASS UNIT

 FIRE ALARM BELL

 EMERGENCY LIGHT

EXIT EXIT SIGN

 NON-RETURN VALVE

5KG CO2
FIRE EXTINGUISHER

⑤ VISUAL FIRE ALARM

 SUBSIDIARY VALVE / FLOW SWITCH

 SPRINKLER CONTROL VALVE SET GATE VALVE

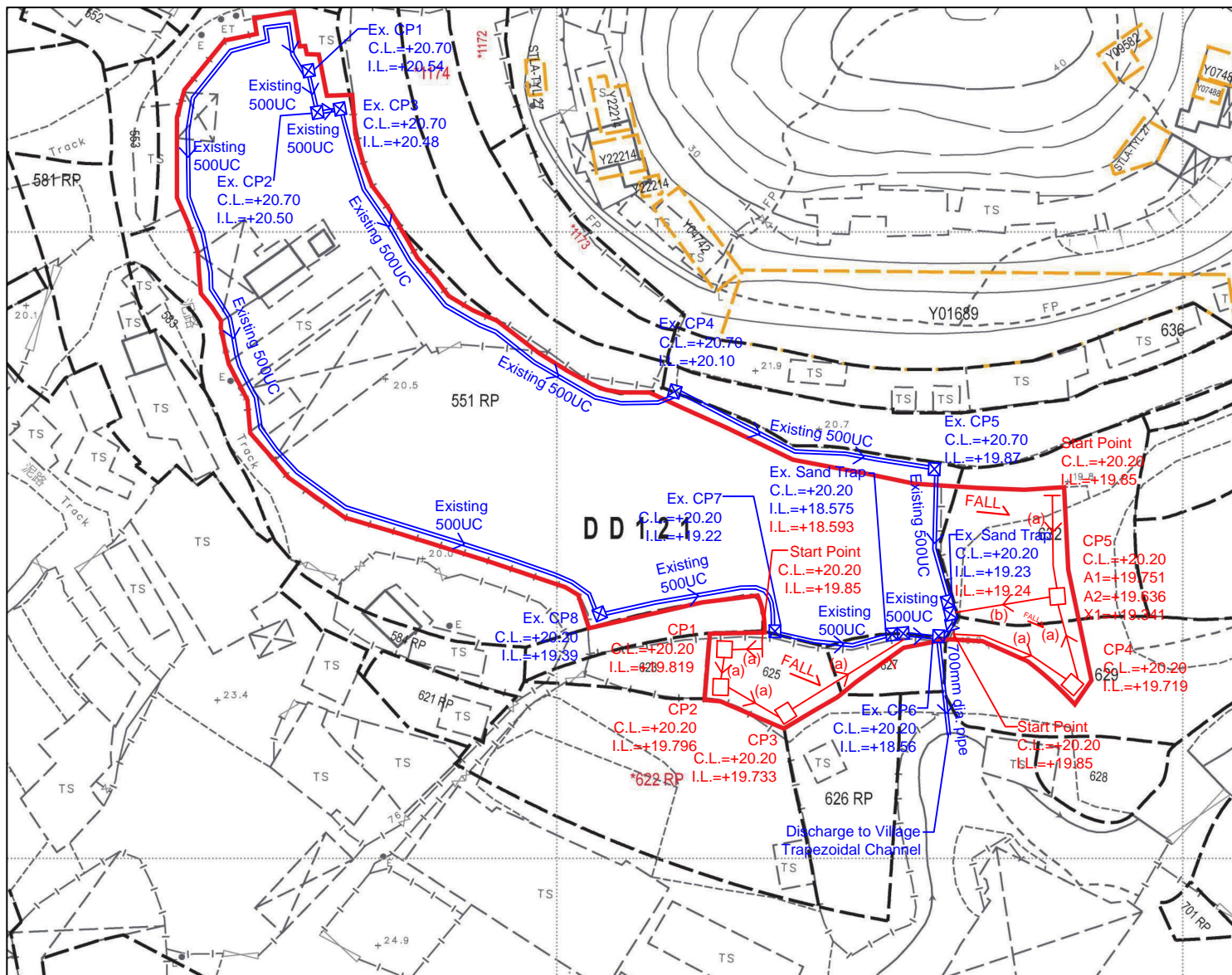
GATE TYPE (With MONITORING)

 PUMP SET Y-TYPE STRAINER SPRINKLER INLET PRESSURE GAUGE

—S— SPRINKLER HEAD (ON PLAN)

5KG DRY POWDER
FIRE EXTINGUISHER

[illegible]

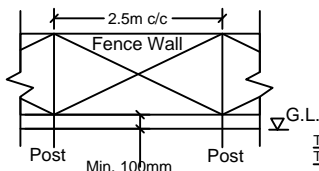


Note:

1. This Drainage Proposal is designed based on the Drainage Proposal for Planning Application A/YL-TYST/1234 (as attached in Appendix A).

2. Catchpit and UC follows Typical Details of Geotechnical Manual for Slope Fig.8.10 and Fig.8.11 respectively.

3. Fence wall, if any, shall be of open-bottom type to avoid blocking of overland flow.



TYPICAL DETAIL OF OPEN-BOTTOM TYPE FENCE WALL

LEGEND

- Existing Catch Pit
- Existing 500UC / 700mm dia. pipe
- Proposed Catch Pit
- Proposed 300UC (1:150) with Cast Iron Cover
- Proposed 300mm dia. concrete pipe (1:150)

正宏工程顧問公司

CHING WAN ENGINEERING CONSULTANT COMPANY

Project:

Proposed Temporary Warehouse and Open Storage of Construction Materials for a Period of 3 Years at Lots 551 RP (Part), 625, 626 RP, 627, 629 (Part), 632 (Part) and 635 (Part) in D.D.121 and adjoining Government Land, Tong Yan San Tsuen, Yuen Long, New Territories
(Application No.:A/YL-TYST/1326)

Title:

Drainage Proposal - LAYOUT

D01

Drawn by:

DM

Date:

7-1-2026

Check by:

DM

Scale:

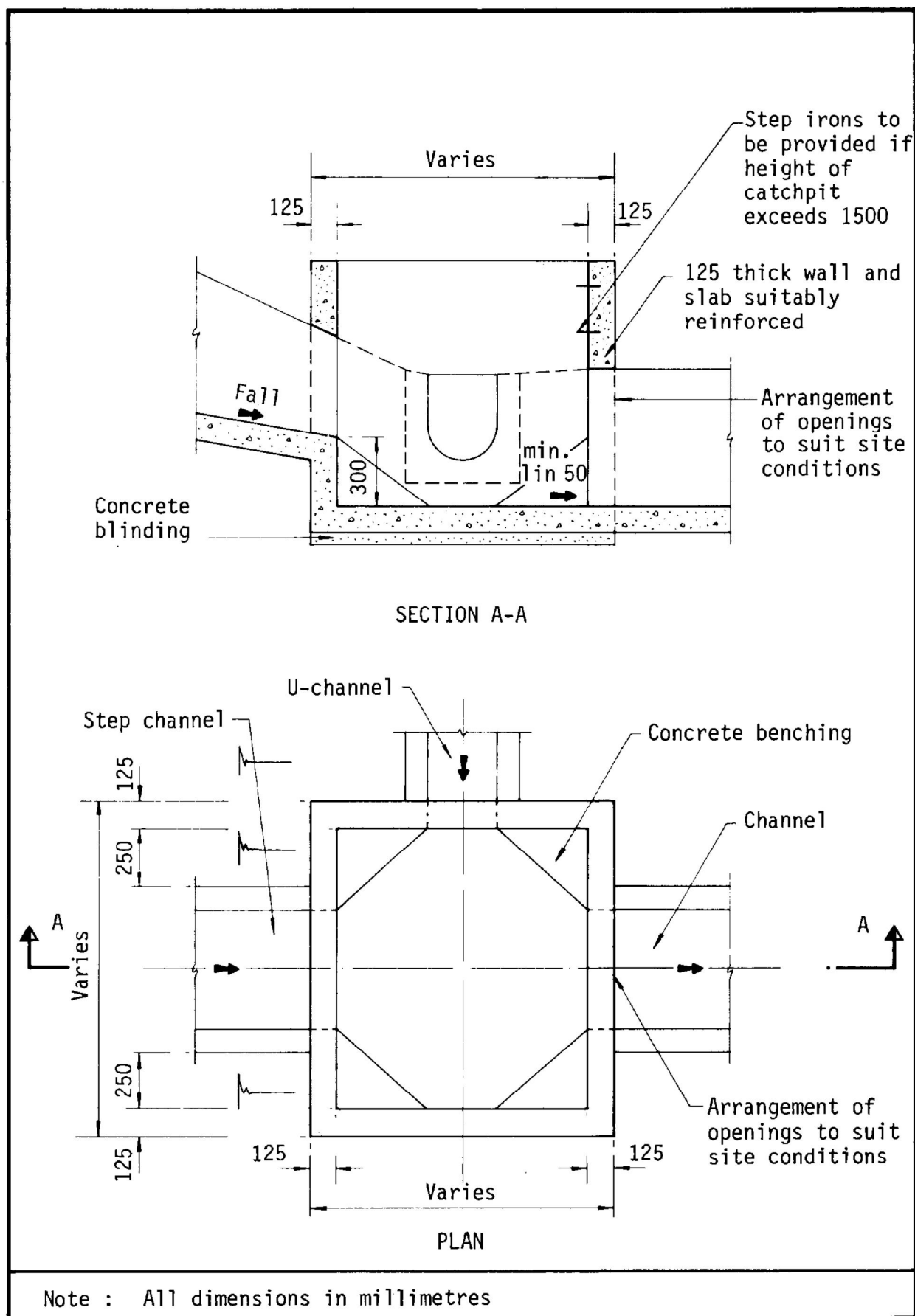
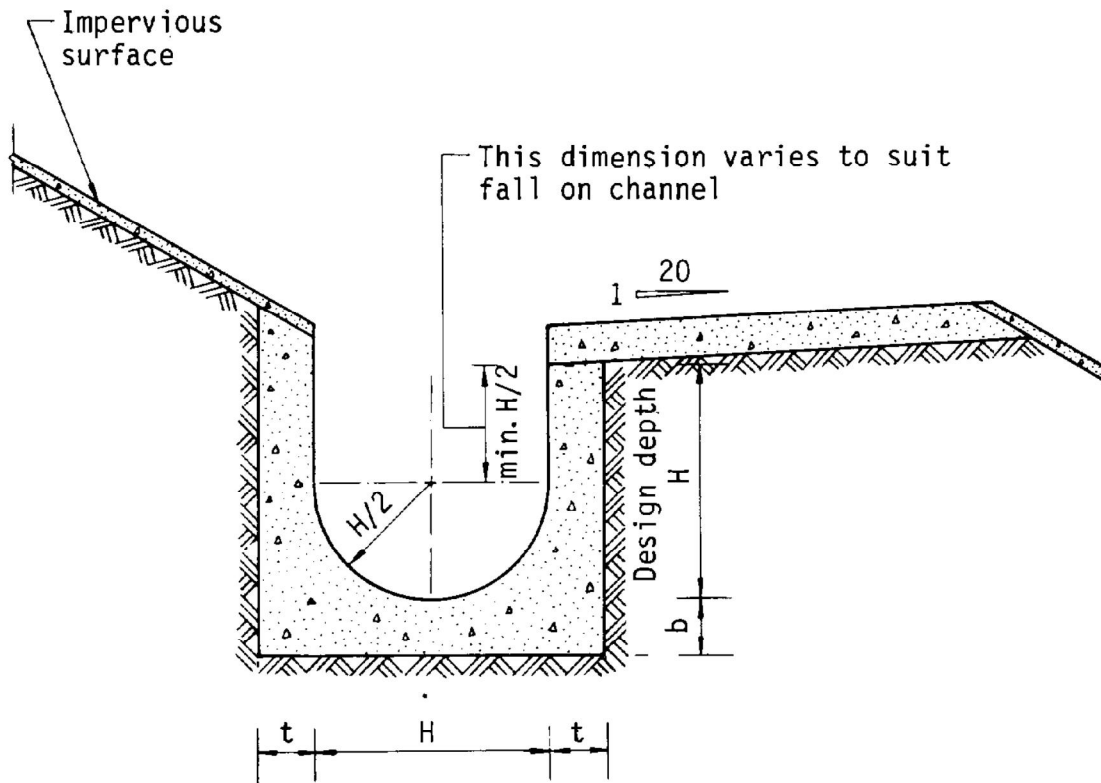


Figure 8.10 - Typical Details of Catchpits



Dimensions of U - channel

Nominal size of channel H (mm)	Thickness t (mm)	Thickness b (mm)
225 to 600	150	150
675 to 1200	175	225

Figure 8.11 - Typical U-channel Details

Appendix A

Drainage Proposal for Planning Application

A/YL-TYST/1234

Project: Proposed Temporary Logistics Centre for a Period of 3 Years
LOT 551 (PART) IN D.D. 121, TONG YAN SAN TSUEN,
YUEN LONG, NEW TERRITORIES

Calculation of Stormwater Water Pipe Sizing

(According to Cap.123I the number and size of water pipes shall be calculated at the rate of 700 mm² of pipe to every 10 m² of horizontal roofed-over surface.)

Catchment Area of site boundary: Area B =	4970	m ² (approx.)
Catchment Area of adjacent area: Area A =	6082	m ² (approx.)
Total Catchment area : Effective Area A+B=	7762.5	m ² (approx.)
The Effective unpaved area Area A	0.5	
The Effective paved area : Area B	0.95	

B) Collected Run-off

Eff. Catchment area, CA = 7762.5 m² (approx.)
 Rainfal intensity, I = 218 mm/hr
 Rainfal increase 11.1%
 Increase Rainfall intensity I = 242 mm/hr
 (Refence from DSD Stormwater Manual Table 2: 50 years return period & 5 mins duration)
 (Refence from Stormwater Drainage Manual. CORRIGENDUM No. 1/2022. Table 28,
 Mid 21st Century, rainfall increase is 11.1%)

Table 28 – Rainfall Increase due to Climate Change

	Rainfall Increase
Mid 21 st Century	11.1%
End of 21 st Century	16.0%

Maximum run-off, $Q_{rf} = I \times C_A$ (m³/hr)
 $Q_{rf} = 0.24 \text{ m/hr} \times 7762.5 \text{ m}^2$
 $Q_{rf} = 1880.06 \text{ m}^3/\text{hr}$
 $Q_{rf} = 522.24 \text{ L/s}$

Maximum stormwater Run-off discharge = 522.24 L/s

Project: Proposed Temporary Logistics Centre for a Period of 3 Years
LOT 551 (PART) IN D.D. 121, TONG YAN SAN TSUEN,
YUEN LONG, NEW TERRITORIES

Capacity of Stormwater Drain Pipe Calculation

Manning Formula:

$$V = \frac{HMD^{2/3} s^{1/2}}{n}$$

V = Velocity (m/s)

HMD = Hydraulic Mean Depth (m)

A_f = Area of Flow (m²)

R_f = Rain Fall in Litre per second

Q = Volume of Flow (L/s)

D = 0.700 = Pipe Diameter in metre (m)

s = 1 : 250 = Gradient (slope)

n = 0.013 = Manning Friction Coefficient (Refer DSD Sewer Manual Part 1)

Type of Pipe	n
New smooth drain	0.011
Cast iron pipe	0.011
Old sewer	0.012
Concrete pipe	0.013

$$HMD = \frac{A_f}{\text{Wetted perimeter}}$$

Hydraulic Mean Depth (HMD):

$$1/3 \text{ bore: } \frac{A_f}{1.231 * D} = 0.1304$$

$$1/2 \text{ bore: } \frac{A_f}{1.571 * D} = 0.1750$$

$$2/3 \text{ bore: } \frac{A_f}{1.911 * D} = 0.2037$$

$$3/4 \text{ bore: } \frac{A_f}{2.094 * D} = 0.2114$$

$$4/5 \text{ bore: } \frac{A_f}{2.214 * D} = 0.2128$$

$$\text{Full bore: } \frac{A_f}{\pi * D} = 0.1750$$

Area of Flow (A_f):

$$1/3 \text{ bore: } 0.292 * A = 0.11237 \text{ m}^2$$

$$1/2 \text{ bore: } 0.500 * A = 0.19242 \text{ m}^2$$

$$2/3 \text{ bore: } 0.708 * A = 0.27247 \text{ m}^2$$

$$3/4 \text{ bore: } 0.805 * A = 0.30980 \text{ m}^2$$

$$4/5 \text{ bore: } 0.857 * A = 0.32981 \text{ m}^2$$

$$\text{Full bore: } 1.000 * A = 0.38485 \text{ m}^2$$

Apply HMD to Manning Formula,

Velocity (V):

$$1/3 \text{ bore: } V = 1.251 \text{ m/s}$$

$$1/2 \text{ bore: } V = 1.522 \text{ m/s}$$

$$2/3 \text{ bore: } V = 1.684 \text{ m/s}$$

$$3/4 \text{ bore: } V = 1.726 \text{ m/s}$$

$$4/5 \text{ bore: } V = 1.734 \text{ m/s}$$

$$\text{Full bore: } V = 1.522 \text{ m/s}$$

$$Q \text{ (m}^3\text{/s)} = V \times A \text{ (by Continuing Equation)}$$

$$Q \text{ (L/s)} = V \times A \times 1000$$

Volume of Flow (Q):

$$1/3 \text{ bore: } Q = 140.59 \text{ L/s}$$

$$1/2 \text{ bore: } Q = 292.86 \text{ L/s}$$

$$2/3 \text{ bore: } Q = 458.89 \text{ L/s}$$

$$3/4 \text{ bore: } Q = 534.78 \text{ L/s}$$

$$4/5 \text{ bore: } Q = 571.94 \text{ L/s}$$

$$\text{Full bore: } Q = 585.78 \text{ L/s}$$

The Area A+B total discharge is **522.24** L/s, therefore the sewage pipe is running in between 2/3 bore and 3/4 bore at a velocity around 1.705m/s.

Proposed 500mm(W) x 1000mm(D) Channel (CP1 - CP6) discharge capacity Calculation:
(For Adjacent area A= 6082 sqm)

Size of the channel = 500 (W)mm x 1000 (D)mm

Proposed maximum water level for channel = 600 (D)mm

Based on Manning's formula,

$$V = \frac{1}{n} \times m d^{2/3} \times i^{1/2}$$

V = velocity in m/s

md = hydraulic mean depth in metres

i = inclination (proposed fall) 1/200

n = factor in surface condition 0.015

U-Channel sectional area A =	(0.5	x	0.35) +	0.0982
	=	0.2732	m ²			
U-Channel Wetted perimeter P =	0.7	+	0.785			
	=	1.4854	m			
md = A / P =	0.2732	/	1.4854	=	0.18	m
V = 1 / n x	0.18	^{2/3}	x	1/200	^{1/2}	
	=	1.5245	m/s			
Flowrate = V x A						
	=	1.5245	x	0.2732	x	1000
	=	416.45	L/s			

Refer to the channel discharge capacity, the maximum catchment area shall be estimated as below:

Site area = 0.5 x 6082 m² = 3041 m² (effective area)

Rf = Rain Fall in Litre per second(L/s)

ESA = The Effective Surface Area

SA = 6082.0 = Total Surface Area in squared metre (m²)

rf = 242.2 = Rainfall in millimetre per hour(mm/hr)

EP = 50% = The Effective unpaved area

The effective surface area is calculated below:

Rf	=	3041.0	m ² X	242.198	mm/hr /	1000	X	1000
					3600			
	=	204.59	L/s		<	416.45	L/s OK

Therefore, the new proposed 500mm(W) x 1000mm(D) channel (CP1-CP6) is considered capable for site area (Adjacent area A) rainfall discharge 6082 sqm rainfall discharge at 50 year turnover period which is the time of concentration at 5 minutes.

Proposed 500mm(W) x 1000mm(D) Channel (CP8 - CP6)
discharge capacity Calculation: (For Subject Site area B - 4970 sq.m)

Size of the channel = 500 (W)mm x 1000 (D)mm

Proposed maximum water level for channel = 600 (D)mm

Based on Manning's formula,

$$V = 1/n \times md^{2/3} \times i^{1/2}$$

V = velocity in m/s

md = hydraulic mean depth in metres

i = inclination (proposed fall) 1/200

n = factor in surface condition 0.015

U-Channel sectional area A =	(0.5	x	0.35) +	0.0982
	=	0.2732	m ²			
U-Channel Wetted perimeter P =	0.7	+	0.785			
	=	1.4854	m			
md = A / P =	0.2732	/	1.4854	=	0.18	m
V = 1 / n x	0.18	^{2/3}	x	1/200	^{1/2}	
	=	1.5245	m/s			
Flowrate = V x A						
	=	1.5245	x	0.2732	x	1000
	=	416.45	L/s			

Refer to the channel discharge capacity, the maximum catchment area shall be estimated as below:

Site area = 0.95 x 4970 m² = 4721.5 m² (effective area)

Rf = Rain Fall in Litre per second(L/s)

ESA = The Effective Surface Area

SA = 4970.0 = Total Surface Area in squared metre (m²)

rf = 242.2 = Rainfall in millimetre per hour(mm/hr)

EP = 95.0% = The Effective paved area

The effective surface area is calculated below:

Rf	=	4721.5	m ² X	242.198	mm/hr /	1000	X	1000
					3600			
	=	317.65	L/s		<	416.45	L/s OK

Therefore, the new proposed 500mm(W) x 1000mm(D) channel (CP8-CP6) is considered capable for subject site 4970 sqm rainfall discharge at 50 year turnover period which is the time of concentration at 5 minutes.

Estimation of Existing River Discharge Capacity Calculation:

Size of the channel = 2500 (W)mm x 1700 (D)mm

Proposed maximum water level for channel = 1400 (D)mm

Based on Manning's formula,

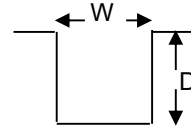
$$V = 1/n \times m d^{2/3} \times i^{1/2}$$

V = velocity in m/s

md = hydraulic mean depth in metres

I = inclination (proposed fall)

n = factor in surface condition 0.06 (for natural channels, very poor condition)



Channel sectional area A	=	2.5	x	1.4
	=	3.5000	m ²	
Wetted perimeter P	=	2.50	+	2.8
	=	5.3000	m	
md	=	A / P	=	3.5000 / 5.3000 = 0.660 m
V	=	1 / n	x	0.660 ^{2/3} x 1/200 ^{1/2}
	=	0.8937	m/s	
Flowrate	=	V x A		
	=	0.8937	x	3.5000 x 1000
	=	3127.97	L/s	or 3.13 m ³ /s

Refer to the channel discharge capacity, the maximum catchment area shall be estimated as below:

Max. area = 0.5 x 92000.0 m² = 46000 m² (effective area)

Rf = Rain Fall in Litre per second(L/s)

ESA = The Effective Surface Area

SA = 92000.0 = Maximum catchment Area in squared metre (m²)

rf = 242.2 = Rainfall in millimetre per hour(mm/hr)

EP = 50% = The Effective unpaved area

The effective surface area is calculated below:

$$Rf = \frac{46000.0 \text{ m}^2 \times 242.198 \text{ mm/hr} / 1000}{3600} \times 1000$$

$$= 3094.75 \text{ L/s} < 3127.97 \text{ L/s} \dots\dots\dots \text{OK}$$

Total Effective Catchment area A&B = 7762.5 m² (approx.)

Total rainfall discharge from A&B = 522.24 L/s

Total rainfall discharge from A&B are only occupy 16.70 % of existing river handling capacity

Therefore, the existing 2500mm(W) x 1200mm(D) existing river is considered have large spare capacity for subject site area rainfall discharge at 50 year turnover period which is the time of concentration at 5 minutes.